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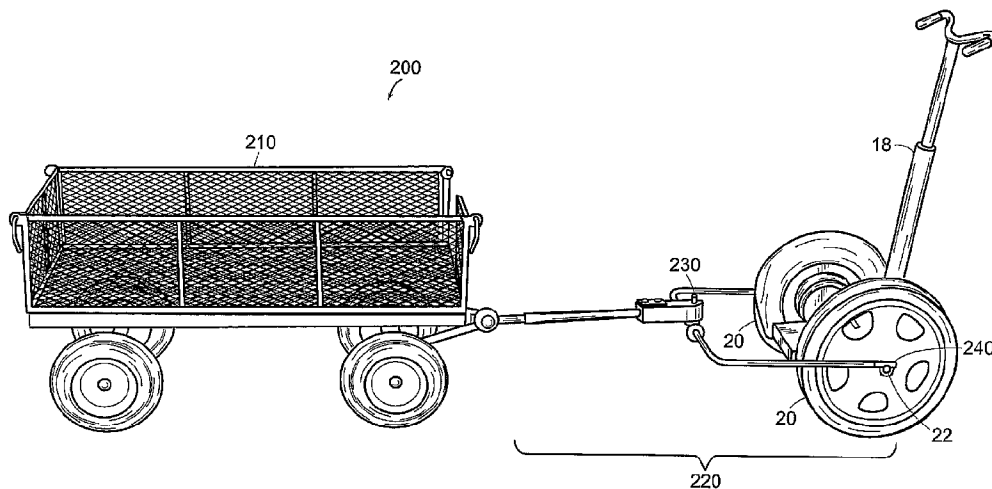
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(54) Title: METHOD FOR ATTACHING A CARRIER TO A BALANCING TRANSPORTER



(57) Abstract: A method for attaching a carrier, such as a trailer (210), to a dynamically balanced transporter (18). The carrier is attached to the transporter with a pivot (240). The pivot axis of the carrier is coincident with the axis of rotation (22) of the wheels (20) of the transporter. This method of attachment minimizes the impact of the trailer (210) on the ability of the transporter (18) to maintain dynamic balance and control.

Method for Attaching a Carrier to a Balancing Transporter

Technical Field

The present invention pertains to carriers, such as trailers, that may be attached to
5 a balancing transporter and, more particularly, to an attachment mechanism that permits
tilting action of the balancing transporter.

Background

Dynamically balancing transporters refer to personal vehicles having a motion
control system that actively maintains the stability of the transporter while the transporter
10 is operating. The motion control system maintains the stability of the transporter by
continuously sensing the orientation of the transporter, determining any corrective action
to maintain stability, and commanding the wheel motors to make the corrective action.
One such transporter is described in U. S. Patent ser. no. 6,302,230. Other dynamically
balancing transporters are described in U. S. Patent ser. nos. 5,701,965 and 5,971,091.
15 Each of these patents is incorporated by reference herein in its entirety.

While control systems for balancing transporters can respond to certain
extraneous torques, the torque presented by a trailer coupled to a balancing transporter in
an arbitrary manner would vary nonlinearly with the orientation of the transporter and
would present an obstacle to stable control of the transporter.

Summary of the Invention

In embodiments of the present invention, a carrier is pivotally attached to a
dynamically balancing transporter with a hitch. The axis of the hitch's pivotal
attachment to the transporter is made coincident with the rotational axis of the
transporter's wheels. Thus, the hitch exerts zero torque about the rotational axis of the
25 wheel minimizing the impact to the dynamic balance of the transporter.

In a specific embodiment of the invention, the carrier is attached to the
transporter such that the carrier is disposed behind the transporter. In another
embodiment of the invention, the carrier is disposed in front of the transporter.

In another embodiment of the invention, a chain of balancing transporters and carriers is provided. A given transporter or carrier is pivotally attached to the carrier or transporter immediately in front of and behind the given transporter or carrier. The pivot axis of any connection to a balancing transporter in the chain is made coincident with the rotational axis of the transporter's wheels. In this way, the impact on the dynamic balance of each transporter is minimized.

Brief Description of the Drawings

The foregoing features of the invention will be more readily understood by reference to the following detailed description, taken with reference to the accompanying drawings, in which:

Fig. 1 is a perspective view of a personal transporter lacking a stable static position, in accordance with a preferred embodiment of the present invention, for supporting or conveying a subject who remains in a standing position thereon;

Fig. 2 shows an illustrative diagram of an idealized balancing transporter with a rigid wheel in motion at a constant velocity across a flat surface;

Fig. 3 illustrates the control strategy for a simplified version of Fig. 1 to achieve balance using wheel torque;

Fig. 4 shows a transporter with attached trailer according to an embodiment of the invention;

Fig. 5 shows a view of the trailer hitch attachment for one wheel of the embodiment of fig. 4;

Fig. 6 illustrates trailer hitch attachment inboard of the transporter wheels;

Fig. 7 shows a front-facing view of the rear of the transporter with the trailer hitch attached;

Fig. 8 shows a transporter with a trailer hitch attached according to an embodiment of the invention;

Fig. 9 shows that the transporter can rotate freely in the aft direction with the trailer hitch attached;

Fig. 10 shows that the transporter can rotate freely in the forward direction with the trailer hitch attached, in the embodiment shown in fig. 8;

Fig. 11 illustrates a method of attaching the hitch arms of the embodiment shown in of figs. 8-10 to the transporter; and

Fig. 12 illustrates a carrier attached to the front of the transporter, according to an embodiment of the invention.

Detailed Description of Specific Embodiments

Definitions: as used in this description and the accompanying claims, the
5 following terms shall have the meanings indicated, unless the context otherwise requires:

A “wheel” is any ground contacting member that is capable of rotation on an axis.

A “carrier” is any platform that is capable of carrying a payload which is suspended on at least one wheel. Carriers include, without limitation, trailers, carts
10 (whether preceding or following an attached transporter) and even other transporters. A carrier may be powered or unpowered.

A “fore-aft plane” will mean a plane that is perpendicular to the rotational axis of a ground contacting element and that contains a vertical line thru a point of ground contact of the ground contacting element. The term “lateral plane” will mean a plane
15 that is parallel to the rotational axis of a ground contacting element and that contains a vertical line thru a point of ground contact of the ground contacting element

A “dynamically balancing (or balanced) transporter” will mean a transporter that lacks static stability in at least a fore-aft plane.

An alternative to operation of a statically stable transporter is that dynamic
20 stability may be maintained by action of the user, as in the case of a bicycle or motorcycle or scooter, or, in accordance with embodiments of the present invention, by a control loop, as in the case of the human transporter described in U.S. Patent ser. no. 5,701,965. The invention may be implemented in a wide range of embodiments. A characteristic of many of these embodiments is the use of a pair of laterally disposed
25 wheels to suspend the subject over the surface with respect to which the subject is being transported. The ground or other surface, such as a floor, over which a transporter in accordance with the invention is employed may be referred to generally herein as the “ground.” The wheels are typically motor-driven. In many embodiments, the configuration in which the subject is suspended during locomotion lacks inherent
30 stability at least a portion of the time with respect to a vertical in the fore-aft plane but is relatively stable with respect to a vertical in the lateral plane. Stability, as defined below,

means that in response to a perturbation a stable device will tend towards its unperturbed state.

Motion Control of a Balancing Transporter

In various embodiments of a balancing transporter, fore-aft stability may be achieved by providing a control loop, in which one or more motors are included, for operation of a motorized drive in connection with the wheels. In these embodiments, the wheels are driven by the motorized drive in the control loop in such a way as to maintain, when the transporter is not in locomotion, the center of mass of the transporter above the region of contact of the wheels with the ground, regardless of disturbances and forces operative on the transporter.

A wheel typically has a "point" (actually, a region) of contact or tangency with the surface over which the transporter is traveling or standing. Due to the compliance of the wheel, the "point" of contact is actually an area, where the region of contact may also be referred to as a contact patch. The weight of the transporter is distributed over the contact region, giving rise to a distribution of pressures over the region, with the center of pressure displaced forward during forward motion. The distribution of pressures is a function both of the composition and structure of the wheel, the rotational velocity of the wheel, the torque applied to the wheel, and thus of the frictional forces acting on the wheel.

A force in the direction of motion is required to overcome rolling friction (and other frictional forces, including air resistance). Gravity may be used, in accordance with preferred embodiments of the invention, to provide a torque about the point of contact with the surface in a direction having a component in the sense of desired motion. Referring to Fig. 2, to illustrate these principles, a diagram is shown of the forces acting on a transporter that locomotes with constant velocity v on a single wheel over a flat surface. The principles now discussed may readily be generalized to operation on a sloped surface and to accommodate any other external forces that might be present. Wheel **160** of radius R_w rotates with respect to chassis **162** about axle **164** and contacts the underlying surface at point **P**. For purposes of illustration only, it is assumed that wheel **160** contacts the surface at a point.

The wheel is driven with respect to the transporter by a torque T (supplied by a motor, for example) which in turn creates a reaction torque $-T$ on the transporter. Since

the torque acts about the axle **164**, the reaction torque corresponds to a force F_b acting at the center of gravity (CG) of the system, including the transporter and payload, where $F_b = T/R_{CG}$, where R_{CG} is the distance between the axle and the CG of the system. The line **170** from the CG to point P is at an angle θ_s relative to the vertical **172**.

5 The rolling friction, f , acting on the wheel at point P, is proportional to the velocity v of the rim of the wheel, with the proportionality expressed as $f = \mu v$. For constant velocity to be maintained, this force f must be exactly canceled. Consequently, with gravity providing the force, the condition that must be satisfied is:

$$F_b \cos \theta_s = f_b, \quad (\text{Eqn. 1})$$

10 where f_b is the component of the reaction force acting transverse to axis **174** between the CG and point P. In order to prevent the transporter from falling, a stability condition must also exist, namely that no net force acts on the CG in a direction transverse to line **170**, i.e., there is no net torque about the point of contact **P** during motion at constant velocity (i.e., in an inertial frame of reference where the point P is
15 fixed). This condition may be expressed as:

$$F_g \sin \theta_s = f_b, \quad (\text{Eqn. 2})$$

where $F_g \sin \theta_s$ is the "tipping" component of gravity, and f_b is the counter-tipping component of the reactive force on the transporter caused by wheel rotation ($f_b = F_b \cos \theta$), and where θ is the angle shown line **170** and line **174**.

20 Eqns. 1 and 2 may be combined to yield $F_g \sin \theta_s \cos \theta_s = f = \mu v$, thus, in the limit of small angles (where $\sin \theta$ is approximately θ),

$$\theta_s = (\mu/F_g) v, \quad (\text{Eqn. 3})$$

showing that increasing velocity requires increased lean to overcome the effects of friction. Additionally, a control loop that imposes stability on the system will respond
25 to an increased lean by increasing velocity of the system. While the preceding discussion assumed constant velocity, additional lean beyond that required to overcome the effects of friction will result in acceleration since an additional forward-directed force acts on the CG. Conversely, in order to achieve acceleration (or deceleration) of the transporter, additional leaning (forward or backward) must be provided in a manner discussed in
30 further detail below.

Fig. 1 shows a simplified embodiment of a balancing transporter. A personal transporter is shown and designated generally by numeral **18**. A subject **10** stands on a support platform **12** and holds a grip **14** on a handle **16** attached to the platform **12**, so

that the transporter **18** of this embodiment may be operated in a manner analogous to a scooter. A control loop may be provided so that leaning of the subject results in the application of torque to wheel **20** about axle **22** thereby causing an acceleration of the transporter. Transporter **18**, however, is statically unstable, and, absent operation of the control loop to maintain dynamic stability, subject **10** will no longer be supported in a standing position. Different numbers of wheels may advantageously be used in various embodiments of the invention as particularly suited to varying applications. Thus, as described in greater detail below, the number of wheels may be any number equal to, or greater than, one. For many applications, the dimensions of platform **12**, and indeed of the entire ground-contacting module, designated generally by numeral **6**, are advantageously comparable to the dimensions of the footprint or shoulder width of user **10**. Thus transporter **18** may advantageously be used as a mobile work platform or a recreational transporter such as a golf cart, or as a delivery transporter.

Operation of the balancing transporter will be described with reference to the set of coordinate axes shown in Fig. 1. Gravity defines the vertical axis **z**, while the axis coincident with the wheel axis **22** may be used to define a lateral axis **y**, and a fore-aft axis **x** is defined by the forward direction of motion of the transporter. Directions parallel to the axes **x** and **y** are called the fore-aft and lateral directions respectively. It can be seen that the transporter, when relying on the pair of wheels **20** for contacting the ground, is inherently unstable with respect to a vertical in the fore-aft direction, but is relatively stable with respect to a vertical in the lateral direction. In other embodiments of the invention described below, the transporter may also be unstable with respect to yaw about the **z** axis.

A simplified control algorithm for achieving balance in the embodiment of the invention according to Fig. 1 when the wheels are active for locomotion is shown in the block diagram of Fig. 3. The plant **61** is equivalent to the equations of motion of a system with a ground contacting module driven by a single motor, before the control loop is applied. **T** identifies the wheel torque. The remaining portion of the figure is the control used to achieve balance. The boxes **62** and **63** indicate differentiation. To achieve dynamic control to insure stability of the system, and to keep the system in the neighborhood of a reference point on the surface, the wheel torque **T** in this embodiment is governed by the following simplified control equation:

$$T = K_1(\theta - \theta_0) + K_2(\dot{\theta} - \dot{\theta}_0) + K_3(x - x_0) + K_4(\dot{x} - \dot{x}_0) \quad (\text{Eqn. 4})$$

where:

- T denotes a torque applied to a wheel about its axis of rotation;
- θ is a quantity corresponding to the lean of the entire system about the ground contact, with θ_0 representing the magnitude of a system pitch offset, all as discussed in
5 detail below;
- x identifies the fore-aft displacement along the surface relative to a fiducial reference point, with x_0 representing the magnitude of a specified fiducial reference offset;
- a dot over a character denotes a variable differentiated with respect to time; and
- 10 • a subscripted variable denotes a specified offset that may be input into the system as described below; and
- K_1 , K_2 , K_3 , and K_4 are gain coefficients that may be configured, either in design of the system or in real-time, on the basis of a current operating mode and operating conditions as well as preferences of a user. The gain coefficients may be of a positive,
15 negative, or zero magnitude, affecting thereby the mode of operation of the vehicle, as discussed below. The gains K_1 , K_2 , K_3 , and K_4 are dependent upon the physical parameters of the system and other effects such as gravity. The simplified control algorithm of Fig. 3 maintains balance and also proximity to the reference point on the surface in the presence of disturbances such as changes to the system's center of mass
20 with respect to the reference point on the surface due to body motion of the subject or contact with other persons or objects. It should be noted that the amplifier control may be configured to control motor current (in which case torque T is commanded, as shown in Fig. 3) or, alternatively, the voltage applied to the motor may be controlled, in which case the commanded parameter is velocity.

25 The effect of θ_0 in the above control equation (Eqn. 4) is to produce a specified offset θ_0 from the non-pitched position where $\theta=0$. Adjustment of θ_0 will adjust the vehicle's offset from a non-pitched position. As discussed in further detail below, in various embodiments, pitch offset may be adjusted by the user, for example, by means of a thumb wheel 32, shown in Fig. 1. An adjustable pitch offset is useful under a variety of
30 circumstances. For example, when operating the vehicle on an incline, it may be desirable for the operator to stand erect with respect to gravity when the vehicle is stationary or moving at a uniform rate. On an upward incline, a forward torque on the wheels is required in order to keep the wheels in place. This requires that the user push

the handle further forward, requiring that the user assume an awkward position. Conversely, on a downward incline, the handle must be drawn back in order to remain stationary. Under these circumstances, θ_0 may advantageously be manually offset to allow control with respect to a stationary pitch comfortable to the user.

5 The size of K_3 will determine the extent to which the transporter will seek to return to a given location. With a non-zero K_3 , the effect of x_0 is to produce a specified offset $-x_0$ from the fiducial reference by which x is measured. When K_3 is zero, the transporter has no bias to return to a given location. The consequence of this is that if the transporter is caused to lean in a forward direction, the transporter will move in a forward
10 direction, thereby maintaining balance. Such a configuration is discussed further below.

 The term "lean" is often used with respect to a system balanced on a single point of a perfectly rigid member. In that case, the point (or line) of contact between the member and the underlying surface has zero theoretical width. In that case, furthermore, lean may refer to a quantity that expresses the orientation with respect to the vertical (i.e.,
15 an imaginary line passing through the center of the earth) of a line from the center of gravity (CG) of the system through the theoretical line of ground contact of the wheel. While recognizing, as discussed above, that an actual wheel is not perfectly rigid, the term "lean" is used herein in the common sense of a theoretical limit of a rigid wheel. The term "system" refers to all mass caused to move due to motion of the wheels with
20 respect to the surface over which the transporter is moving.

 "Stability" as used in this description and in any appended claims refers to the mechanical condition of an operating position with respect to which the system will naturally return if the system is perturbed away from the operating position in any respect.

25 Acceleration of the transporter may be established by system lean. For example, to achieve forward acceleration of the transporter by forward system lean; the center of gravity of the system (transporter and payload) would be placed forward of the center of the pressure distribution of the contact region where the wheels contact the ground-- the more the lean, the more the acceleration. Thus, furthermore, it can be seen that leaning,
30 in conjunction with gravity and friction, determines acceleration (positive or negative) of the system. In this manner, if the transporter is moving forward, pitching the system back will achieve braking. Because the transporter must overcome friction, there is typically some system lean when the transporter is moving at constant velocity over level ground.

In other words, looking at the torque on the transporter caused by gravity and the torque caused by all other external forces, the torque applied by the motorized drive is adjusted so that the net torque from all these sources produces a desired acceleration.

Carrier Attachment to a Balancing Transporter

5 As described above, dynamic stability for a transporter can be maintained by applying a torque to a wheel about its axis of rotation. Attachment of a carrier to the transporter may be advantageous to increase the payload carrying capacity of the transporter. Such attached carriers must not impact substantially the dynamic stability of the transporter. Generally speaking, any component of a force exerted by the carrier on
10 the transporter that is transverse to the vertical direction must be minimized or particularly accounted for by the control law.

 In an embodiment of the present invention a carrier is pivotally attached to a dynamically balancing transporter with a hitch. The axis of the hitch's pivotal attachment to the transporter is made coincident with the rotational axis of the
15 transporter's wheels. The hitch exerts zero torque about the rotational axis of the wheel thereby minimizing the impact to the dynamic balance and control of the transporter.

 Referring to fig. 4, in an embodiment of the present invention, a system **200**, is provided that includes a dynamically balancing transporter **18** and an attached trailer **210**. The trailer **210** is equipped with a hitch **220** to attach the trailer to the transporter.
20 The hitch **220** includes a "lateral" pivot **230** to allow lateral movement of the transporter relative to the trailer. The hitch also includes "fore-aft" pivots **240** (shown for one of the transporter's wheels **20**) to allow fore-aft movement of the transporter relative to the trailer. The axis of each fore-aft pivot is coincident with the rotational axis **22** of the wheels **20**. This method of attachment ensures that the trailer coupling to the transporter
25 exerts no torque about the rotational axis of the wheels, regardless of the relative fore-aft orientation of the trailer with respect to the transporter. Thus, dynamic balance of the transporter is unaffected by the trailer, as can be seen from eqn. 4. The combination of transporter and trailer allows larger payloads to be carried over a surface than if the transporter was used alone. Fig. 5 shows a detailed view of the trailer hitch attachment
30 for one wheel of the embodiment of fig. 4.

 Referring to fig. 6, in a specific embodiment of the present invention, the fore-aft pivots **340** of the trailer hitch, shown for one wheel, are attached to the transporter **18**

inboard of the transporter wheels **20** (not shown). The axes of the fore-aft pivots are again coincident with the rotational axis **22** of the respective wheel. Fig. 7 shows a front-facing view of the rear of the transporter with the trailer hitch attached. The hitch connection to the trailer is omitted for clarity. This embodiment of the invention
5 advantageously minimizes the combined width of the transporter plus trailer hitch.

In another embodiment of the invention, the trailer hitch is attached to the transporter inboard of the transporter's wheels, as shown in fig. 8. Lateral pivot **430** allows lateral movement with respect to transporter **18** for a trailer attached to the hitch. A horizontal bar **450** attaches to the lateral pivot **430** and attaches rotatably to each of
10 two hitch arms **460**. The hitch arms **460** are shaped as an arc. The hitch arms may be pivotally attached to the transporter **18** at the wheel transmission, as shown in figs. 8-10. As shown in fig. 11, each hitch arm may be attached to a track **480** via a slide assembly **490**. The slide assembly includes ball bearings or the equivalent to allow the hitch arm to slide freely on the track. (The hitch arm is not shown for clarity.) Track **470** is
15 circular with the center of the track at the rotational axis **22** of the wheel. This design ensures that the force of the trailer hitch is over the transporter's wheels at all times, exerting zero torque about the rotational axis of the wheels. Note, that as illustrated in figs. 9 and 10, the arcuate shape of the hitch arms together with the pivots at each end of the arms allow the transporter to rotate freely fore and aft of the horizontal with the
20 trailer attached. In a further specific embodiment of the invention, each hitch arm may be attached at the transporter **18** to a fore-aft pivot with the axis of rotation of the fore-aft pivot coincident with the rotational axis of the wheels.

In other embodiments of the present invention, any number of carriers or balancing transporters may be attached to each other in a chain of carriers or transporters.
25 The attachment of one transporter or carrier to the adjacent transporter or carrier is with a hitch that includes a fore-aft pivot. At each pivotal hitch connection to a balancing transporter, the axis of the fore-aft pivot is made coincident with the rotational axis of the transporter's wheels. This attachment scheme minimizes the effect of the attached carrier or transporter on the balance and control of the transporter to which it is attached.

30 In another embodiment of the invention, as shown in fig. 12, a carrier **400** is attached to a balancing transporter **18** such that the carrier travels in front of the transporter. The carrier is pivotally attached to the transporter with a carrier hitch **420** that can be similar to any of the trailer hitches described above. The carrier hitch may be

attached either inboard or outboard of the transporter wheels. The axis of each carrier hitch fore-aft pivot **550** is coincident with the axis of rotation **22** of the wheels. Lateral pivot **530** allows lateral movement with respect to transporter **18** for the carrier attached to the hitch. The carrier may be suspended on any combination of wheels including a
5 single wheel. For example, the carrier may include caster wheels **410** in front and rear as shown in fig. 11 or may include a single caster wheel in the center of the carrier end nearest the transporter. Alternatively, the carrier may include caster wheels I front and may be suspended by the hitch in the rear.

The described embodiments of the invention are intended to be merely exemplary
10 and numerous variations and modifications will be apparent to those skilled in the art. While the preceding embodiments have been described in terms of use of one or more wheels as a ground contacting element for the transporter and for the carrier(s), other types of ground contacting elements may be employed in embodiments of the invention. The various types of ground contacting elements may be mixed in any combination in
15 various embodiments of the invention. These and other variations and modifications are intended to be within the scope of the present invention as defined in the appended claims.

What is claimed is:

1. A method for governing motion of a combination of a dynamically balanced transporter and a carrier, the method comprising:
 - coupling the carrier to the dynamically balanced transporter with a pivot, the pivot characterized by a pivot axis;
 - tilting the transporter in a direction of desired motion; and
 - governing motion of the combination of transporter and carrier in response to the tilt of the transporter.
2. A method according to claim 1, wherein the carrier is a second transporter.
3. A method according to claim 1, further including:
 - coupling an additional carrier to the carrier.
4. A method according to claim 3 wherein at least one of the carrier and the additional carrier is a transporter.
5. A method according to claim 1 wherein the transporter includes a platform and at least one ground-contacting element, each ground contacting element rotatably attached to the platform about a rotation axis and wherein the pivot axis is coincident with the rotation axis.
6. A method according to claim 5 wherein coupling the carrier includes attaching the carrier such that the carrier rides behind the transporter.
7. A method according to claim 5 wherein coupling the carrier includes attaching the carrier such that the carrier rides in front of the transporter.
8. A method according to claim 5, wherein the transporter includes at least two laterally disposed ground contacting elements and coupling the carrier includes attaching the carrier such that at least one pivot is disposed between two ground contacting elements.

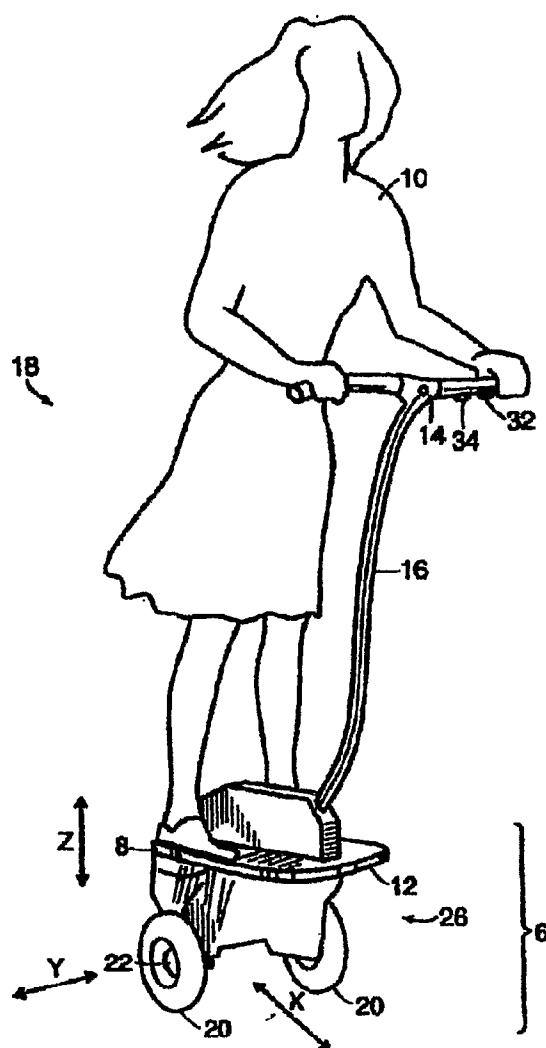


FIG. 1

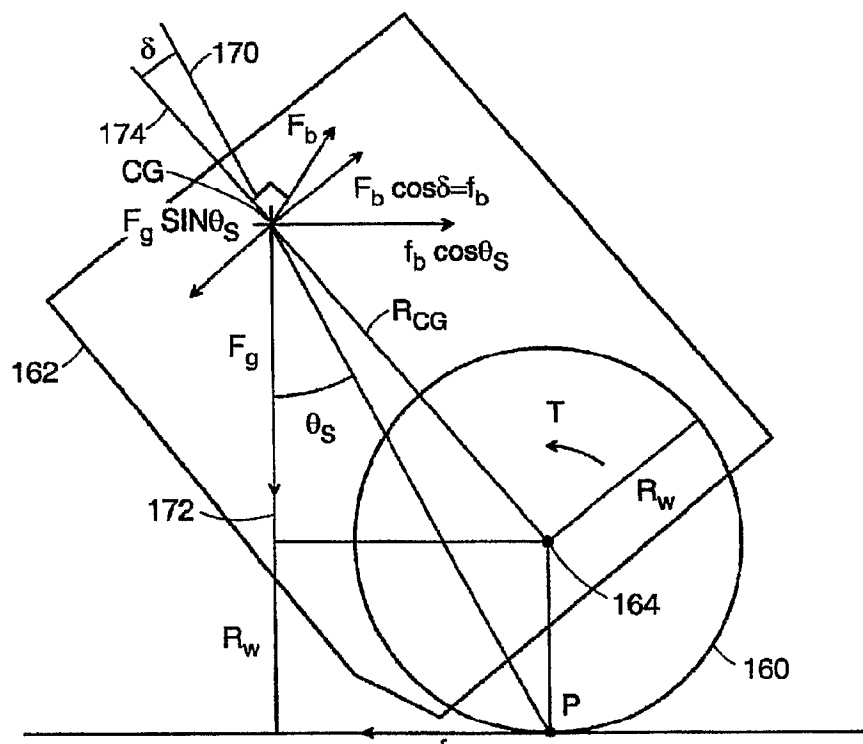


FIG. 2

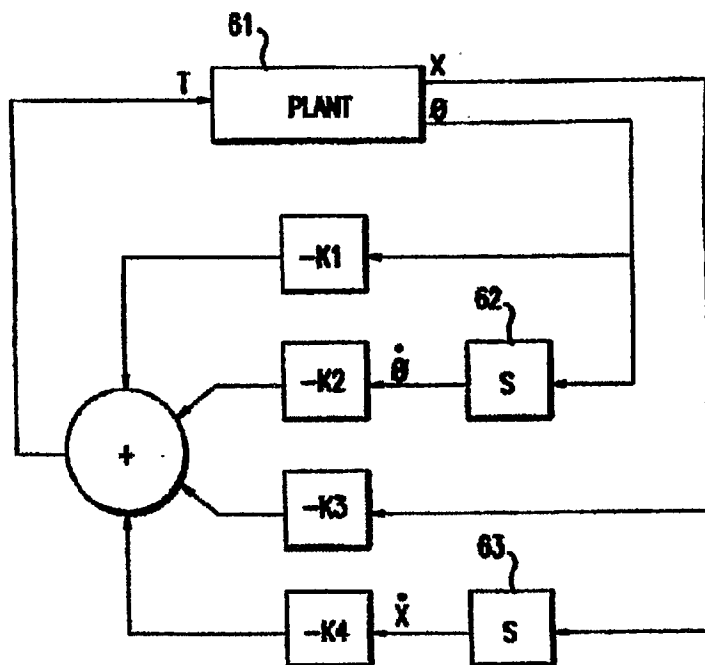


FIG. 3

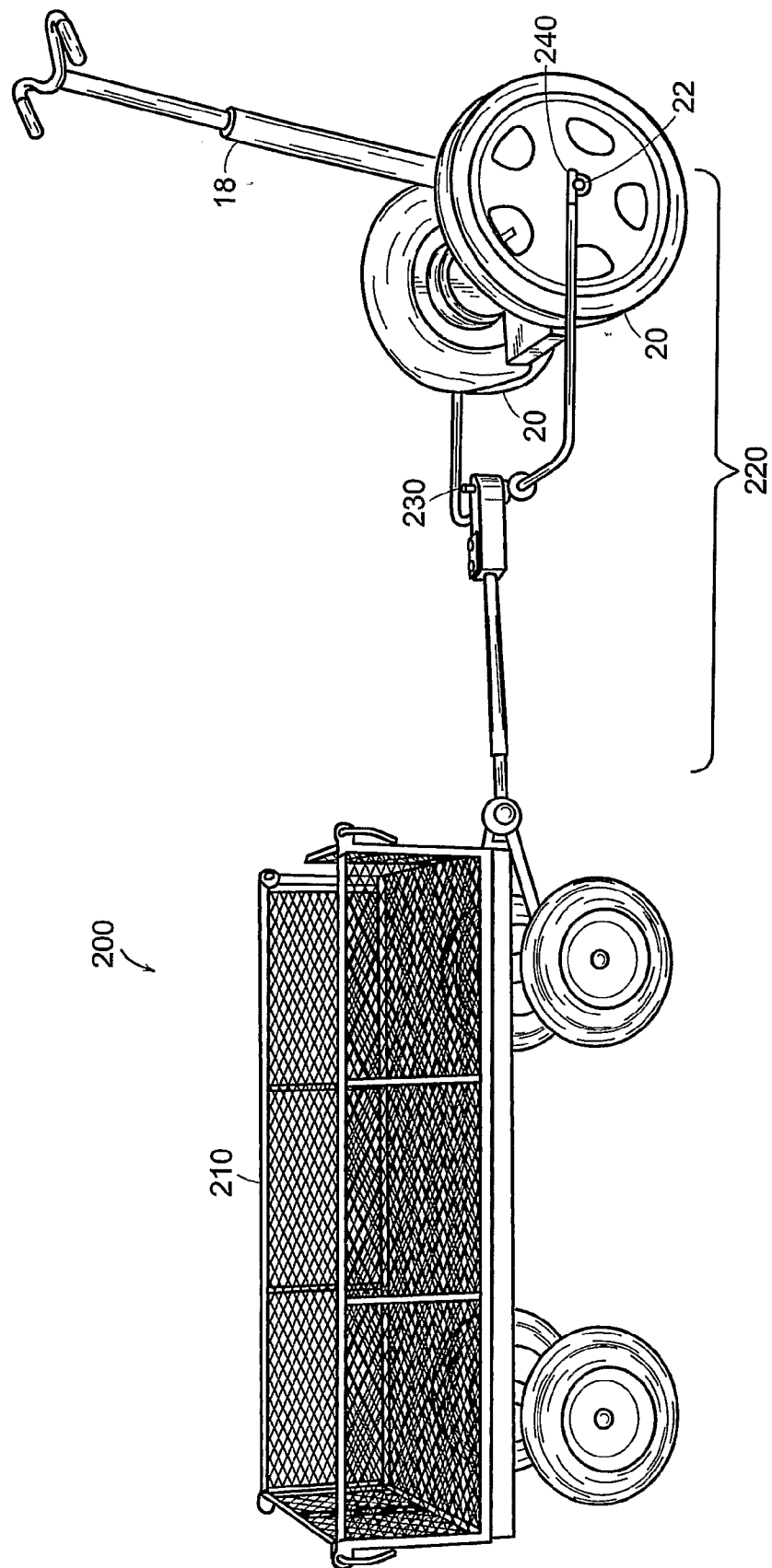


FIG. 4

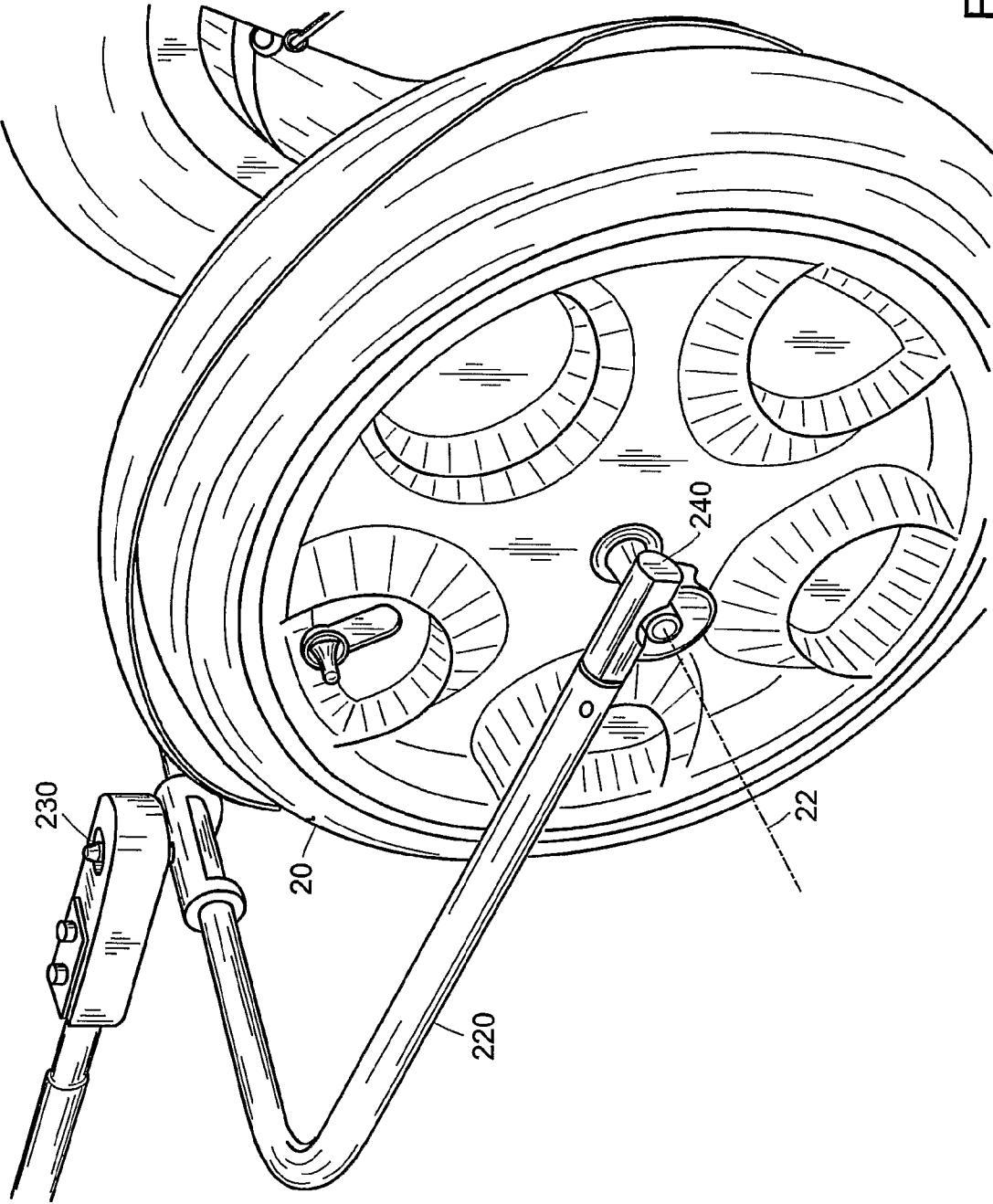


FIG. 5

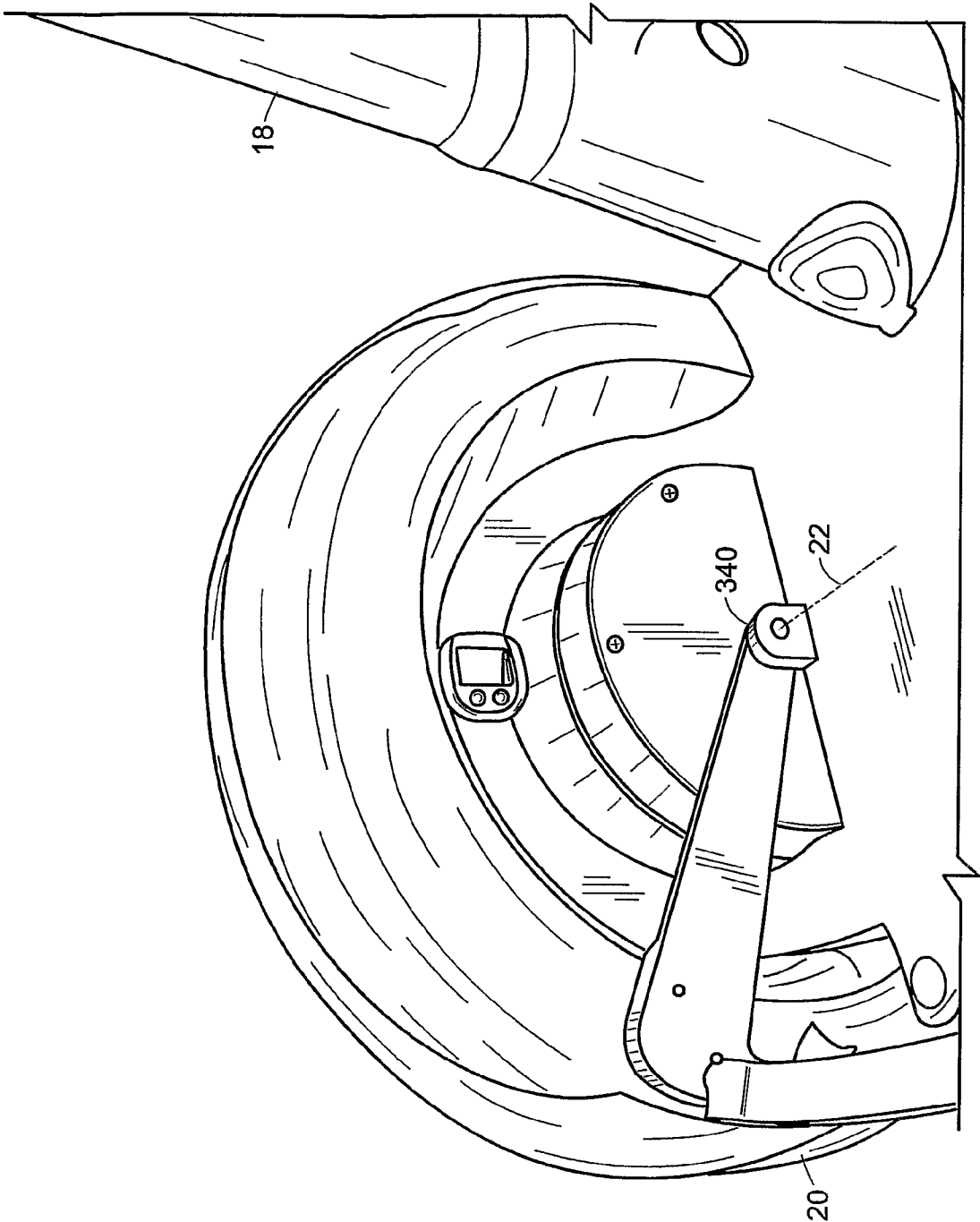


FIG. 6

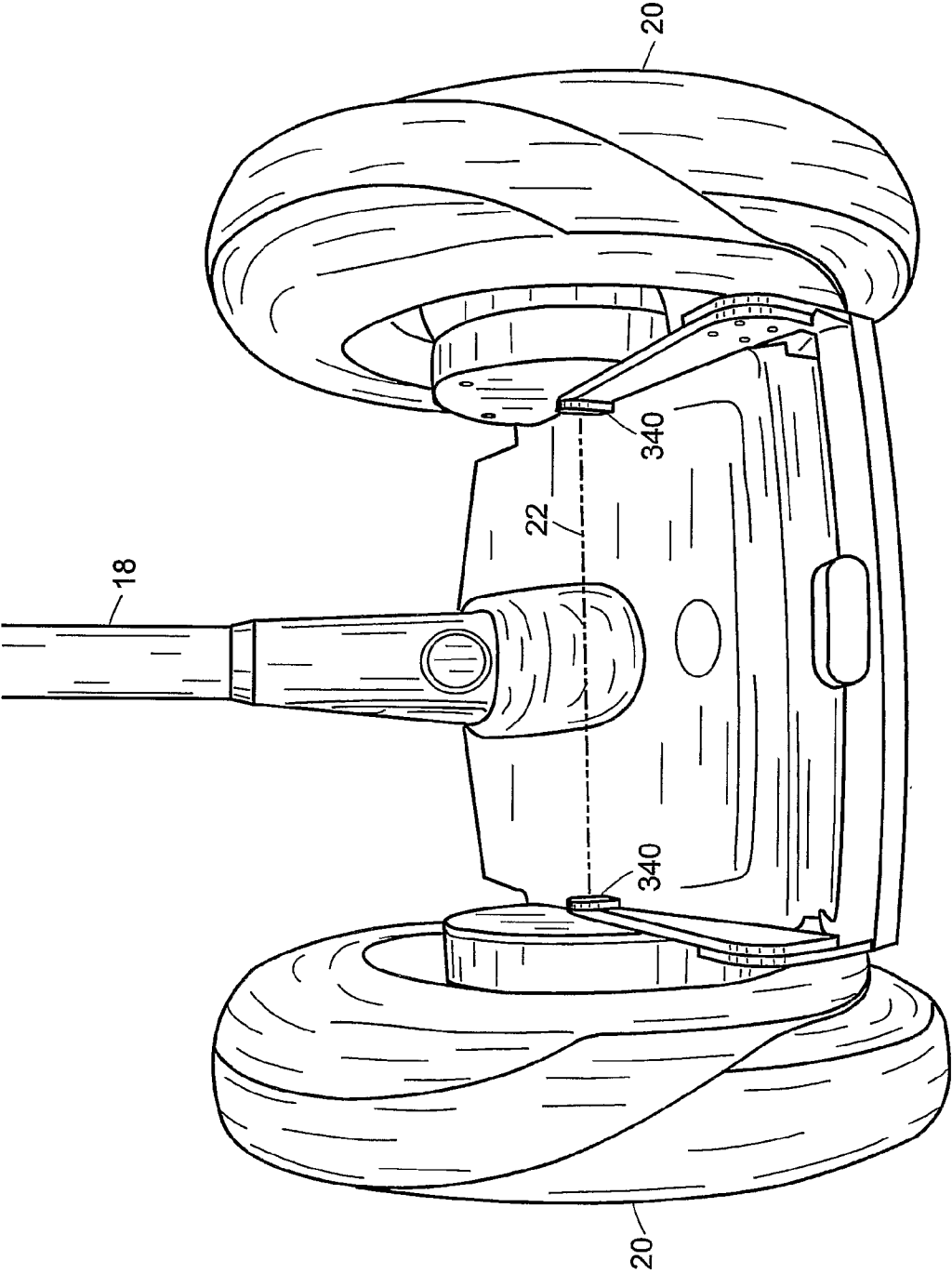


FIG. 7

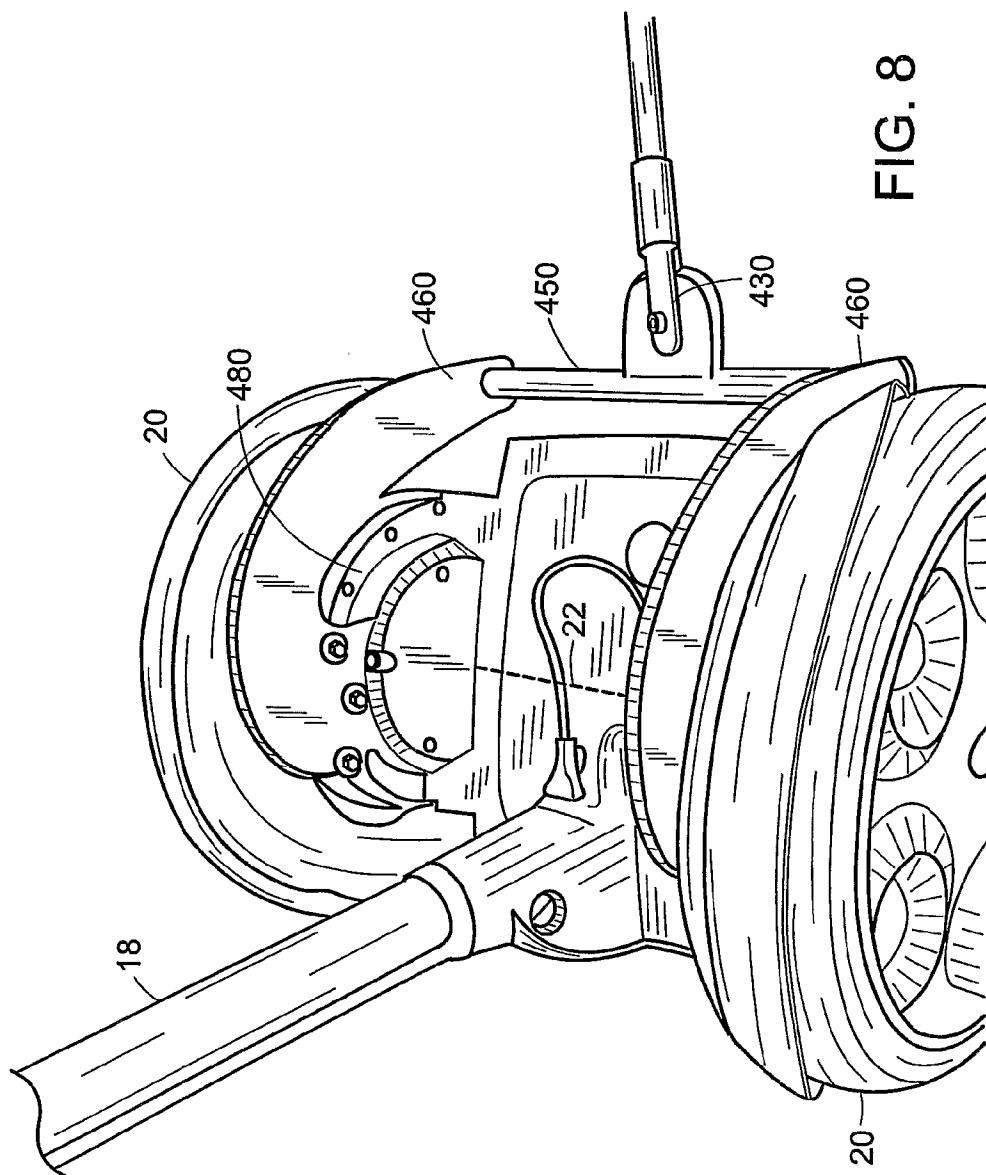
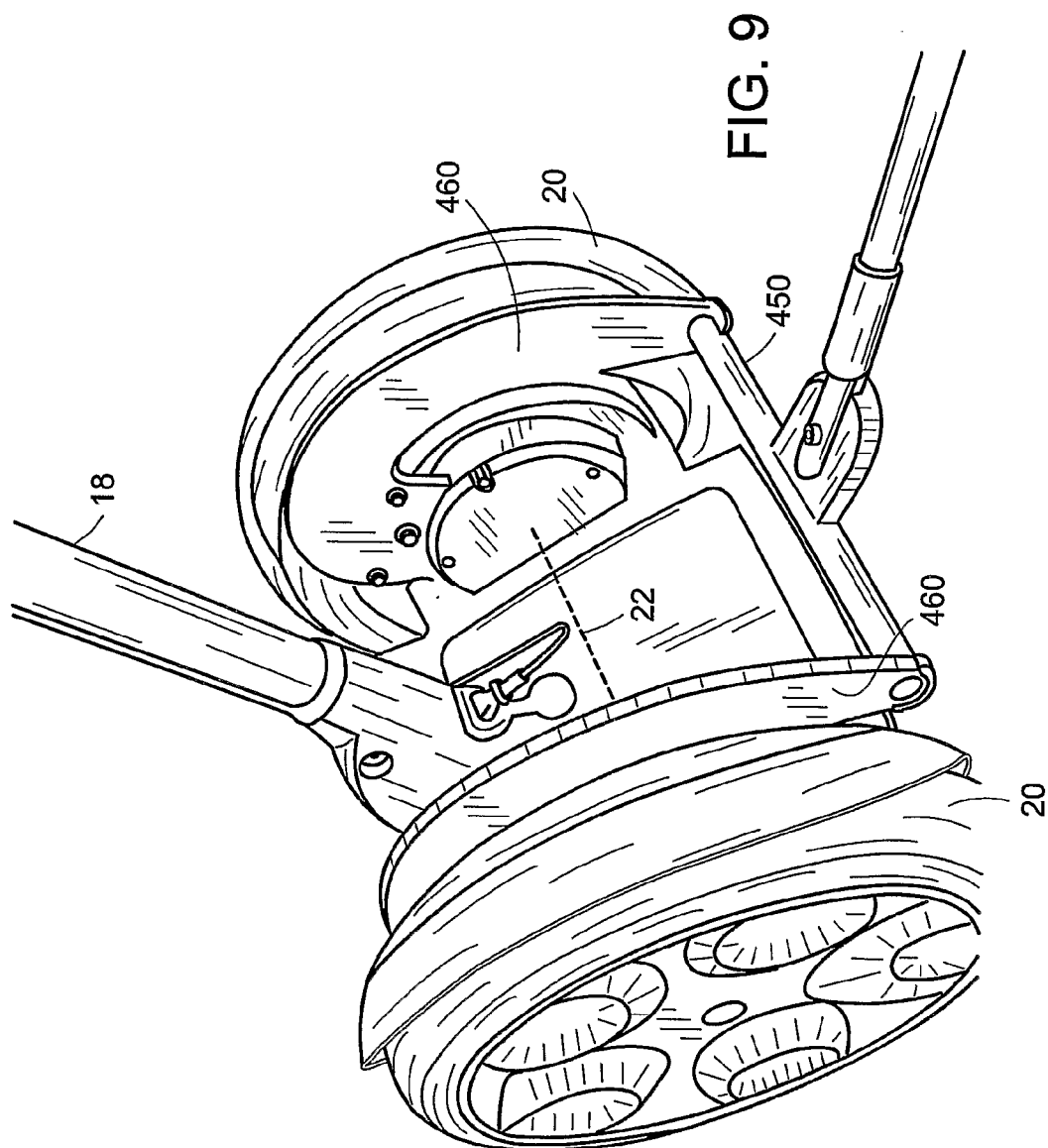
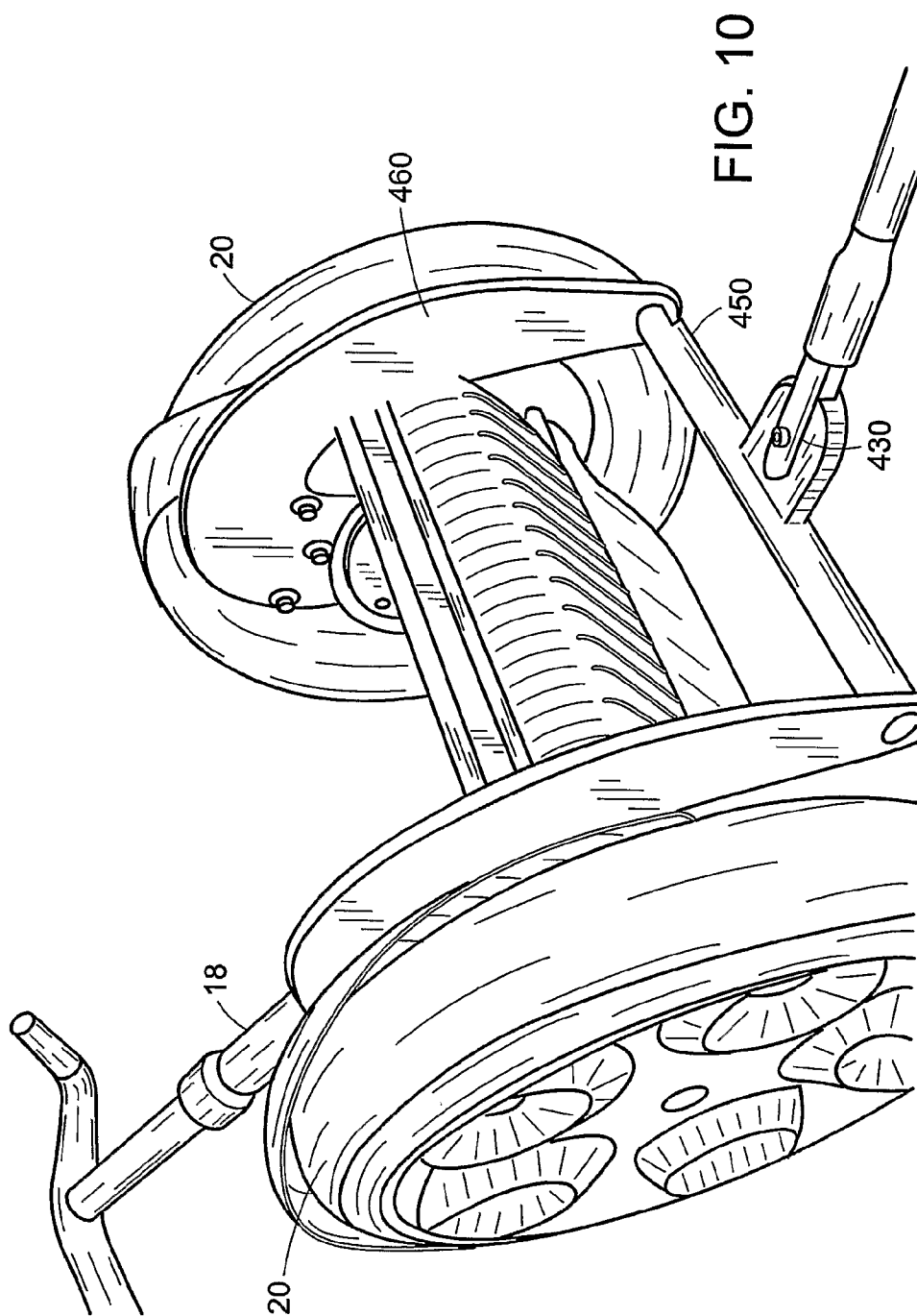
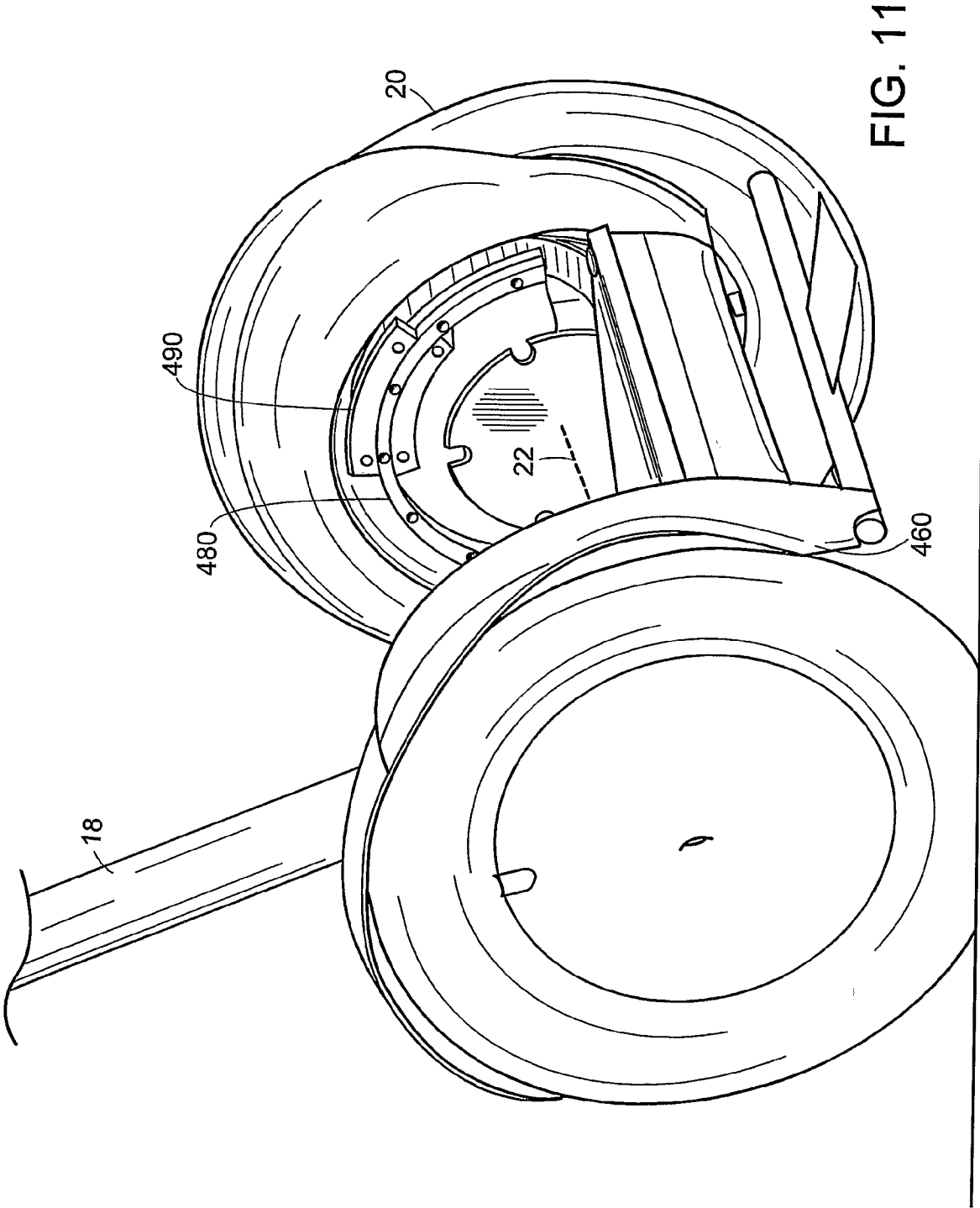
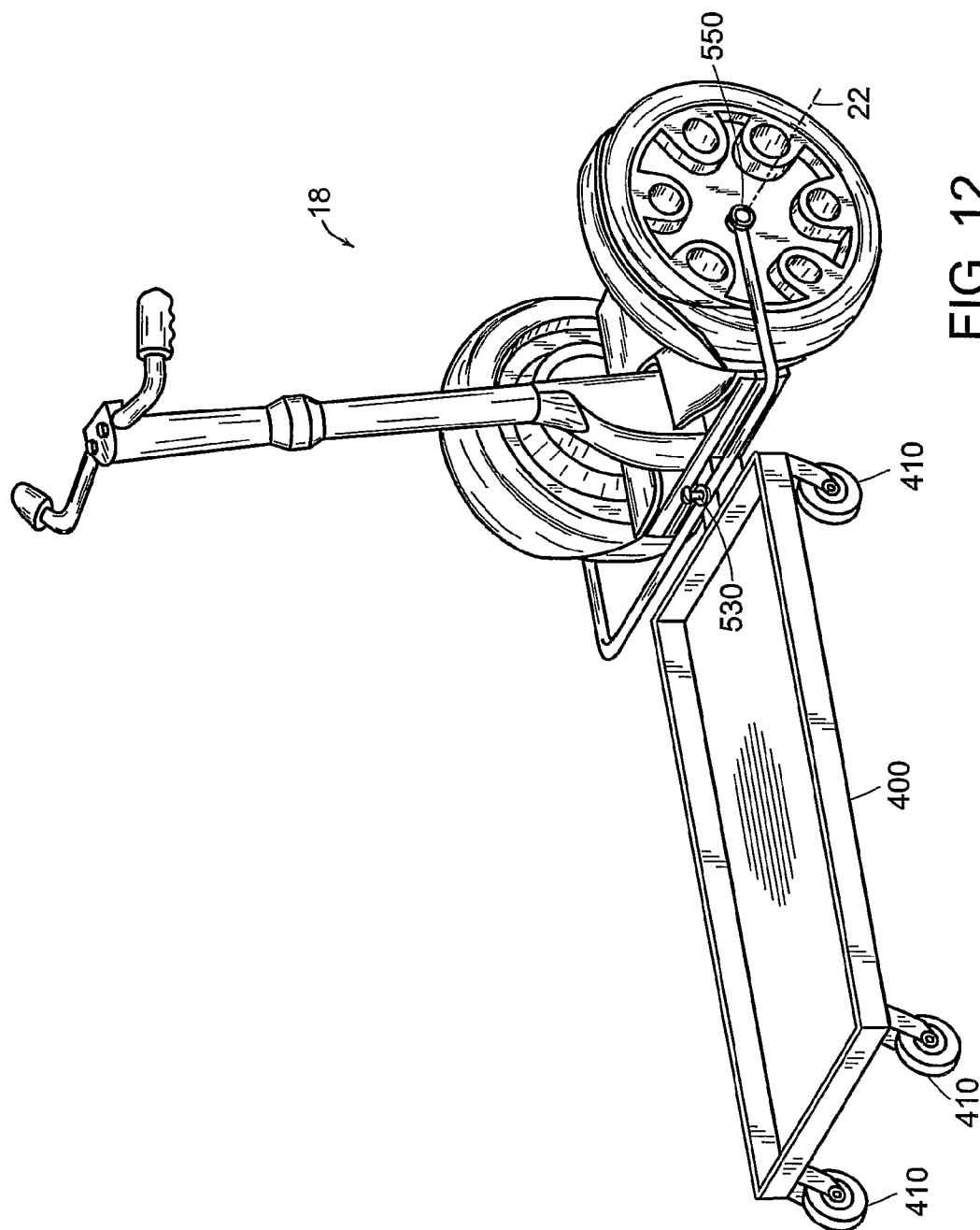


FIG. 8









INTERNATIONAL SEARCH REPORT

International Application No

PCT/US2004/023330

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 B62D51/02 B62D51/00 B62D63/06 B62D53/02

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 B62D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2002/149172 A1 (FIELD J DOUGLAS ET AL) 17 October 2002 (2002-10-17) claims 1-4; figure 2	1-4

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

27 October 2004

Date of mailing of the international search report

05/11/2004

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INTERNATIONAL SEARCH REPORT

International Application No

PCT/US2004/023330

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US 2002149172 A1	17-10-2002	US 6435535 B1	20-08-2002
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